

ISAP- International Workshop on Asphalt Binders and Mastics

Overview of the Use of Fracture Mechanics for Binders and Mastics Characterization

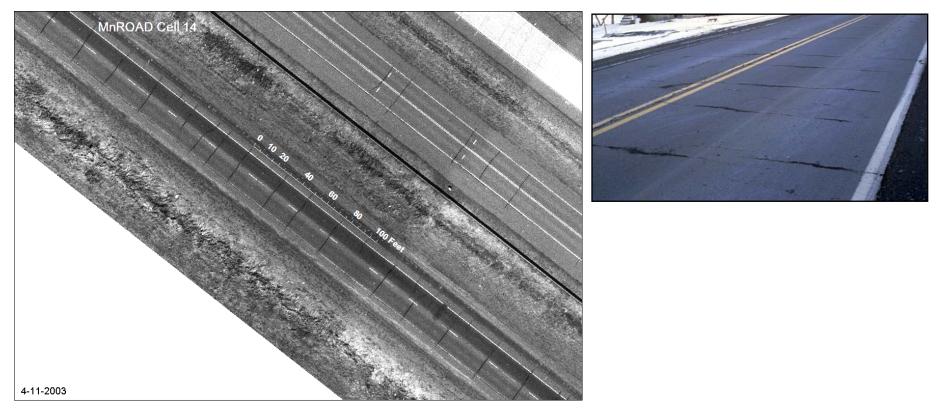
Raul Velasquez, Hussain Bahia, and Hassan Tabatabaee

September 16th,2010 Madison-Wisconsin





Motivation



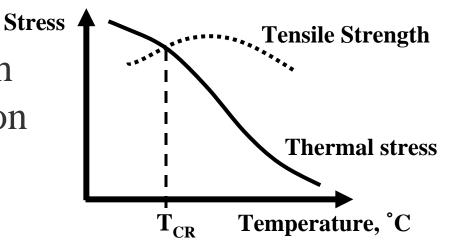
*From Marasteanu class lectures



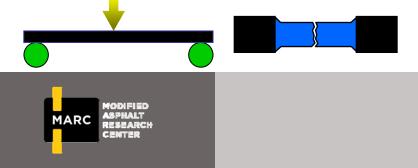


Motivation

Thermal cracking is Str addressed based on strength and creep tests performed on asphalt binders and asphalt mixtures



Two simple laboratory tests were developed by SHRP: (1) Bending Beam Rheometer Test (**BBR**) (2) Direct Tension Test (**DTT**) $\sigma_{ij}(t) = \int_{0}^{t} E_{ijkl}(t-\xi) \frac{\partial \varepsilon_{kl}(\xi)}{\partial \xi}$



$$\sigma_{ij}(t) = \int_{0}^{t} E_{ijkl}(t-\xi) \frac{\partial \mathcal{E}_{kl}(\xi)}{\partial \xi} d\xi$$
$$\mathcal{E}_{ij}(t) = \int_{0}^{t} D_{ijkl}(t-\xi) \frac{\partial \sigma_{kl}(\xi)}{\partial \xi} d\xi$$



Motivation

Mitigation of thermal cracking requires an understanding of relevant parameters that describe how cracks initiate and propagate

- •Most widely used binder test method to address low temperature cracking is **BBR**
- •BBR characterizes material in linear viscoelastic domain at small strain levels and therefore could be limited in its ability to provide a complete picture of thermal cracking phenomenon
 •More appropriate approach is to use test methods based on fracture mechanics principles => such as Single-Edge Notch Beam test (SENB)





Background

➢ Various pavement distresses are related to fracture properties of asphalt layer

≻Longitudinal, thermal, and reflective cracking

Fracture resistance of asphalt materials significantly influences service life of pavements

➤Most powerful tool to study fracture properties of engineering materials is fracture mechanics

Earliest attempts to investigate mechanism of fracture in asphalt was performed by Moavenzadeh (1967)

>It took more than two decades to incorporate fracture mechanics tools in asphalt materials characterization





Background

Fracture strength is function of cohesive forces holding atoms together

Theoretical cohesive strength of brittle and elastic material is $\sim E/10 =>$ Experimentally E/100 to E/10,000

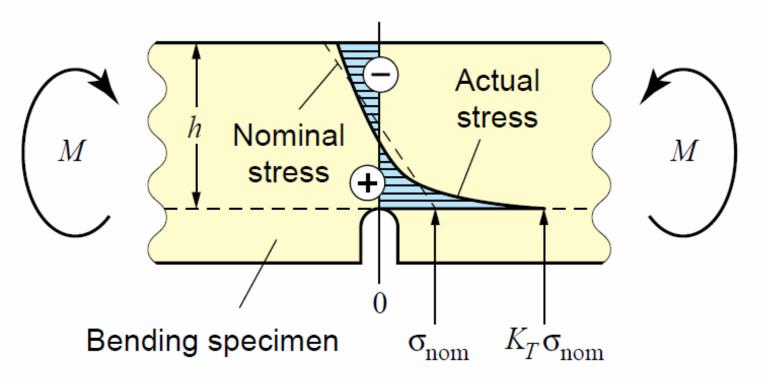
Griffith (1920s) proposed that difference is due to microscopic flaws amplifying local stress and producing stress concentration





Background

Stress-Concentration Effect of Notch in Bending

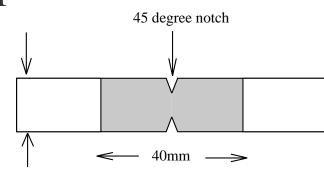




Double Edge Notch Tension Test (DENT)

Andriescu and Hesp (2004) tested binders at 20°C and fracture energy (G_f) was measured to predict fatigue cracking

Essential work of fracture (**EWF**) method was used to estimate fracture resistance of binders by dividing strain energy into essential work of fracture (w_e) and plastic work of fracture (w_p)



30mm

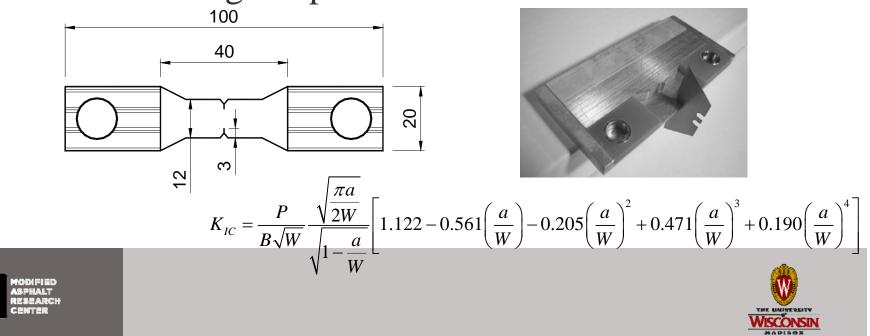




Double Edge Notch Tension Test (DENT)

Zofka and **Marasteanu** (2007) compared **DENT** and **DT** for nine different binders

-Results showed that **DENT** produces better repeatability than **DT** and it can be used to estimate critical cracking temperatures of binders



Lee and Hesp (1994) were among first to use SENB geometry to measure fracture properties of asphalt binders

Anderson et al. (2001) used SE(B) or SENB test to measure fracture toughness of fourteen types of asphalt binders: one plain binder and its thirteen modified ones

They checked effectiveness of characterization of lowtemperature cracking resistance with different grading methods
Fourteen asphalt binders were much better discriminated based on fracture toughness than PG criteria





•SENB results by Olard and Di Benedetto (2004) indicated that fracture toughness was less dependent on temperature and loading rate than fracture energy

•Data showed probable existence of lower bound for fracture energy of asphalt binders => reached in glassy and brittle state of asphalt binders

Asymptotic value for fracture energy of asphalt mixtures was also reported by Li and Marasteanu (2004)





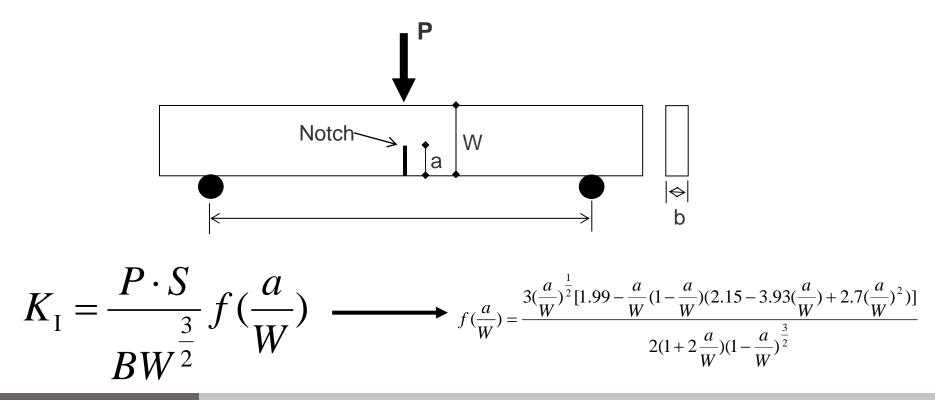
Research by **Hoare and Hesp** 2000, **Hesp** 2003, **Chailleux and Mouillet** 2006, **Chailleux et al**. 2007 have also used SENB to obtain fracture properties of asphalt binders at low temperatures

=> They succeeded in grading a broad range of materials with different levels of modification





Follows ASTM E399 and assumes linear elastic fracture mechanics (LEFM) conditions are true



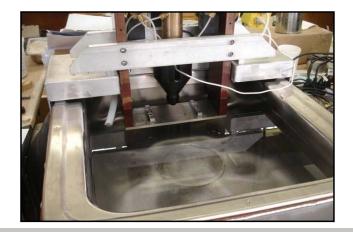




BBR-SENB system



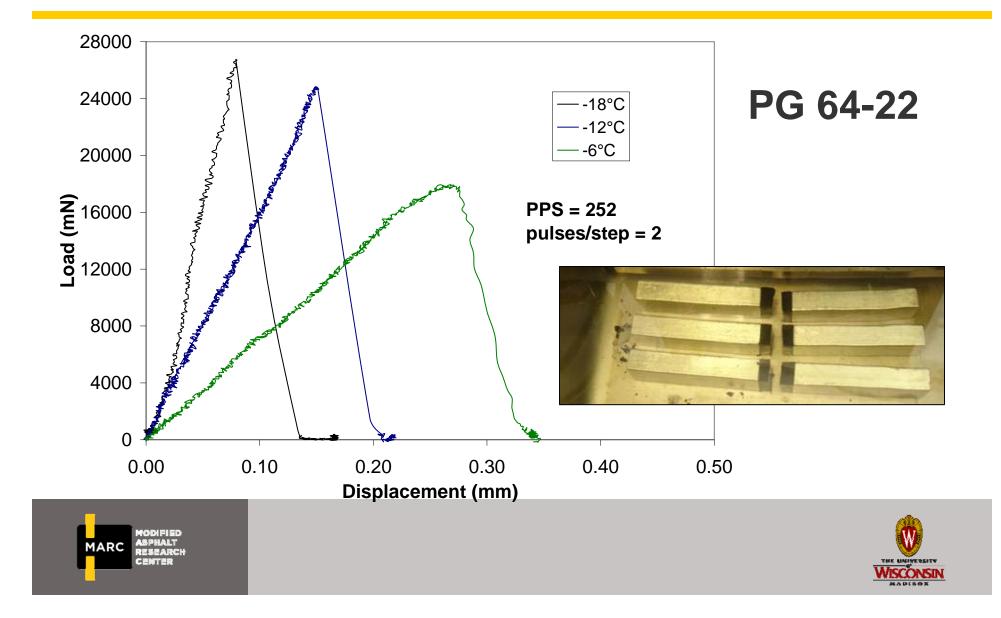






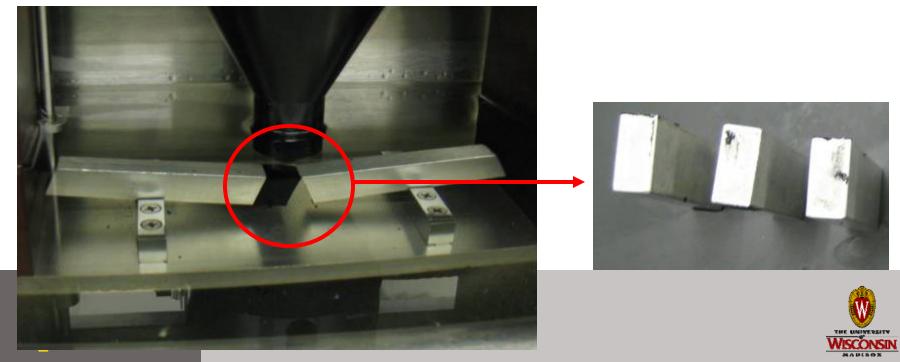


BBR-SENB: Typical Results Binders

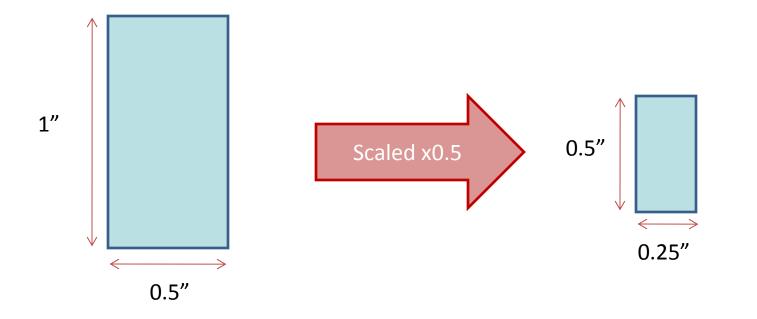


Issues with current SENB Geometry

- Sample preparation is time consuming and difficult
- Adhesion problems
- Samples are delicate and premature failure at metal-binder interface usually occurs when manipulating beams before testing



Proposed Change in Geometry



Original Size

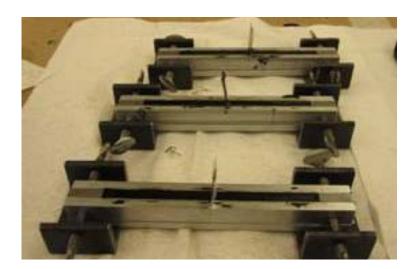
New Size (BBR)





BBR-SENB system

Modification of basic **BBR** testing device was carried out to allow for **controlled deformation rate** and a new SENB sample geometry => **BBR** beam with a notch was used to provide a more homogeneous specimen

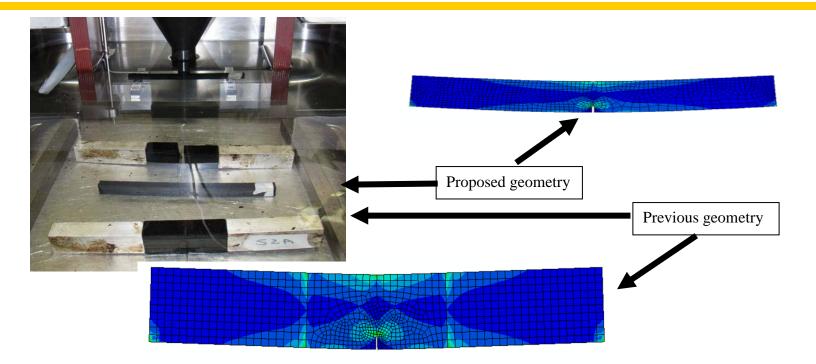








Previous and New Geometry

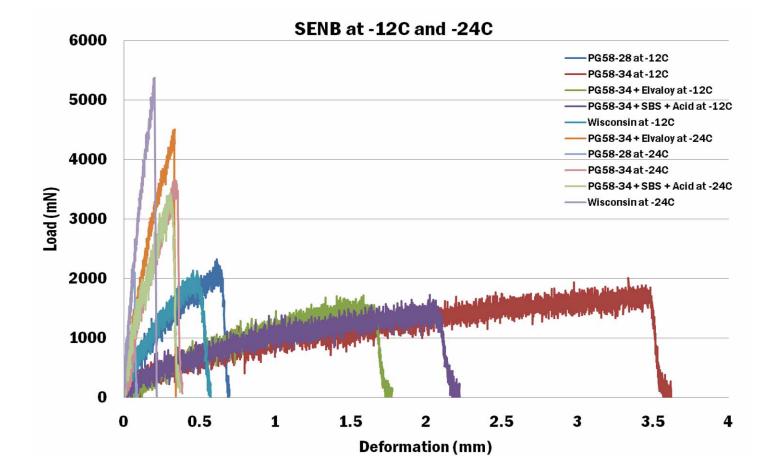


No stress discontinuities are observed proposed geometry. Adhesion problem between binder and metal bars is avoided





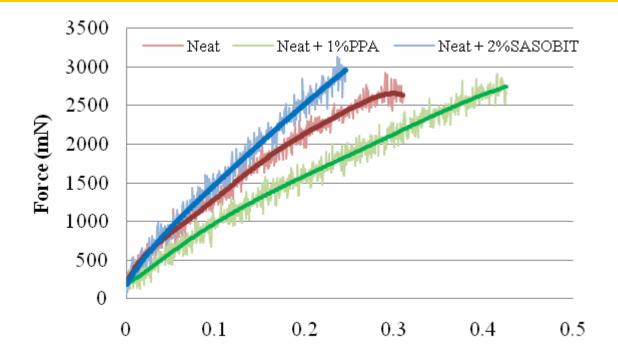
BBR-SENB: Typical Results







BBR-SENB: Typical Results

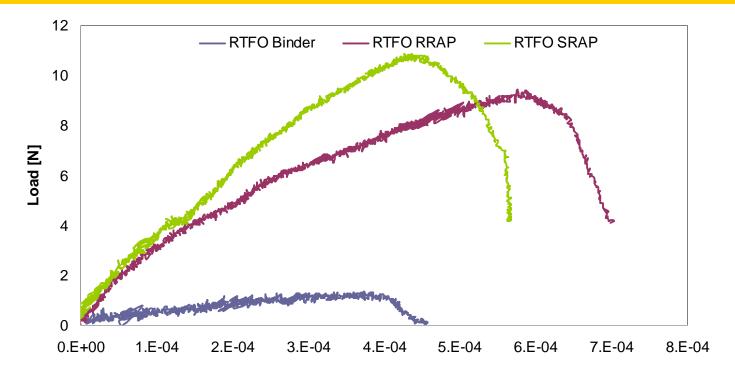


Force-displacement graph for PG 64-22 binder plus modification at -12° C





BBR-SENB: Mastics



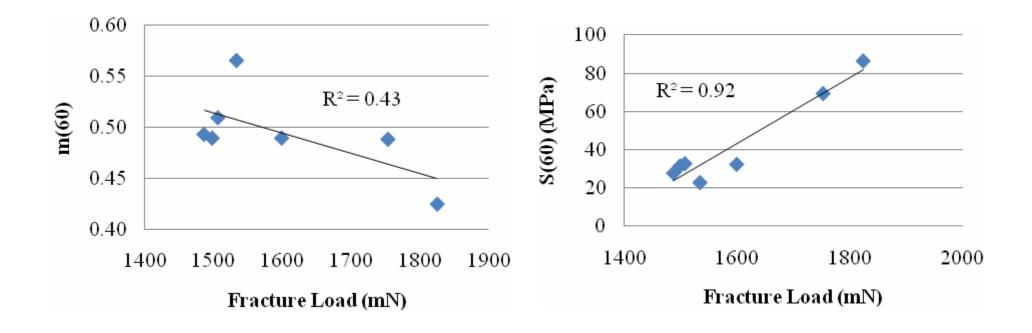
Displacement [m]

System is capable of differentiating fracture properties of RAP materials





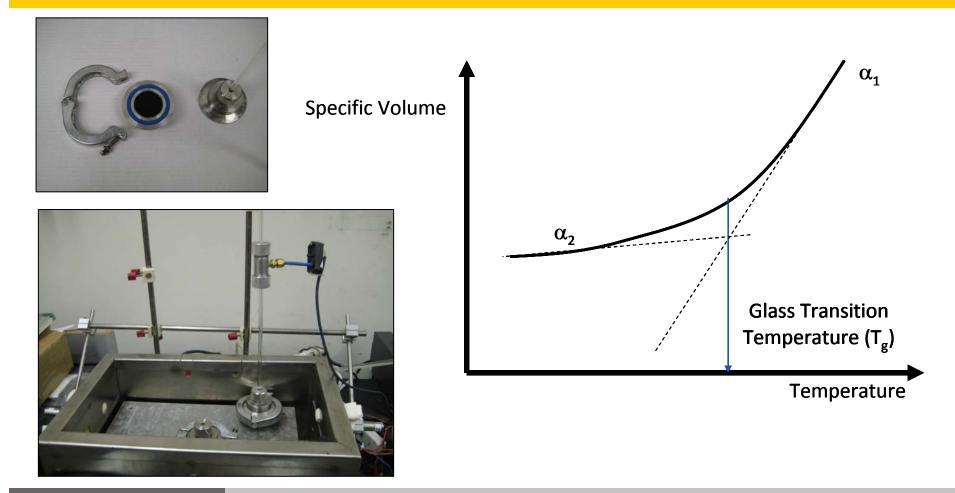
SENB and BBR







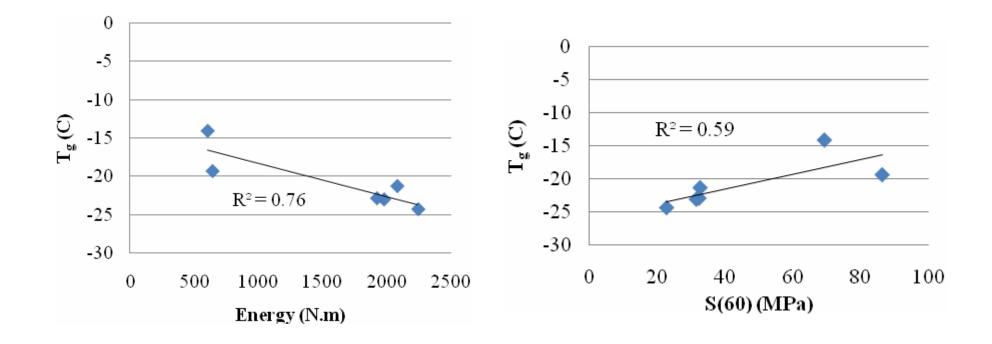
Glass Transition T_g







$\mathbf{T}_{\mathbf{g}}$ and SENB, BBR







Why use fracture mechanics for low temp cracking?

Test Methods in N		ID	State	Asphalt binder
FORCE	Force	IL 174	IL	AC-20
	AG specimen	MN75 2	MN	PG 58-28
AC specimen	()	MN75 4	MN	PG 58-34
		MnROAD 03	MN	PG 58-28
	Transducers	MnROAD 19	MN	PG 64-22
CMOD Transducer		MnROAD 33	MN	PG 58-28
SCD	IDT	MnROAD 34	MN	PG 58-34
FORCE	AC specimen FORCE	MnROAD 35	MN	PG 58-40
AC specimen		US20 6	IL	AC-10
		US207	IL	AC-20
	CMOD Transducer	WI STH 73	WI	PG 58-28
CMOD Transducer				
SENB	DCT			

* Marasteanu et al. (2007) "Pooled Fund Study on Low Temperature Cracking Phase I"





Why use fracture mechanics for low temp cracking?

Laboratory parameters		Correlation coefficients			600								
		Pearson	Spearman	/m^2]	500	<u></u>							
	SCB, fracture energy	-0.708	-0.718	Energy [J/m^2]	400	<u>}</u> `⊗₀;							
	IDT, S(60sec)	-0.713	-0.405		300		♦ ``	· · · ·	<u>ک</u>	♦ 			
Mixture parameters	IDT S(500sec)	-0.590	-0.071	SCB, Fract.	200								
	SCB,Fracture Toughness	-0.639	-0.736	S	100								
	IDT, strength	-0.325	-0.571		0	0	200	400	600	800	1000	1200	1400
	DCT, fracture energy	-0.265	-0.500	┢	1.20			Tran	sverse o	racking	, ft/500ft		
	SEB energy	-0.291	-0.500		(Wba.m0.5)								
Binder parameters	BBR S @ 60sec	0.105	0.248		GN 8 0.80					•			
	m-value S @ 60sec	-0.252	0.152		äuungi 1.60				· • 😖		••••••	•	
	DT strain at 3%	-0.694	-0.673		o 1 0.40	-							
	DENT Stress at failure	-0.045	0.217		0.40 0.20 0.20	-							
	DENT Strain at failure	-0.239	-0.250		0 .00	0	200	400	600	800	1000	1200	1400
				Transverse cracking, ft/500ft									

* Marasteanu et al. (2007) "Pooled Fund Study on Low Temperature Cracking Phase I"





Final Remarks

- **BBR-SENB** test is able to capture ductile-brittle transition =>a good indicator of glass transition of binder
- In contrast to BBR, it is believed that BBR-SENB test can capture effects of non-linear viscoelastic or damage resistance behavior of binders at low temperatures => a potentially ideal performance characterization test





Final Remarks

- Based on LTC phase I experiments
 - -Simple descriptive statistics show that all **fracture parameters** are significant with respect to measured cracking occurrence
 - -Fracture toughness and fracture energy have highest correlations to field performance





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Thank you!



